# Radon daughter plateout background in nEXO – a simulation study

Raymond Tsang, Venkatesh Veeraraghavan, and Andreas Piepke University of Alabama

on behalf of



June 15, 2022

LRT 2022, SDSMT

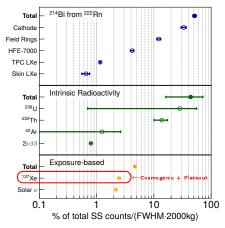
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nEXO Rn daughter plateout

# nEXO backgrounds

- nEXO searches for 0νββ of <sup>136</sup>Xe in a LXeTPC.
- Background sources:
  - Radon outgassing
  - Intrinsic radioactivity
  - Exposure-based background
    - Cosmogenics
    - Dust
    - Radon daughter plateout
- Not a major background, but still on our radar.

#### nEXO Background



nEXO Collaboration, J. Phys. G: Nucl. Part. Phys. 49, 015104 (2022)

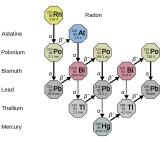
# Rn daughter plateout mechanism

#### Creation of <sup>210</sup>Po:

- Rn daughters plate out on surfaces
- Decay to <sup>210</sup>Pb during assembly
- <sup>210</sup>Pb decays to <sup>210</sup>Bi then <sup>210</sup>Po during operation

Background due to <sup>210</sup> Po:

- Emission of 5.304 MeV  $\alpha$  by <sup>210</sup>Po
- $(\alpha, n)$  reaction in low-Z materials (Z < 14).
- Neutron capture on  $^{136}$ Xe and scattering  $\implies$  background (smaller)
- <sup>137</sup>Xe  $\beta$  decays (Q = 4.173 MeV,  $\tau_{1/2} = 3.8$  mins)  $\implies$  background



Lead

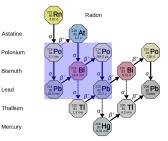
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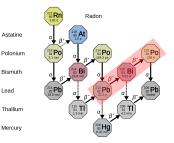
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Lead

# Background rate calculation

The background rate due to  $^{210}$ Po,  $B_{210Po}$ , can be calculated as:

$$B_{210Po} = A_{210Po} \cdot Y_n \cdot \varepsilon_n \cdot \varepsilon_{distrib}$$

where

- A<sub>210Po</sub>: <sup>210</sup>Po activity
- Y<sub>n</sub>: Neutron yield
- $\varepsilon_n$ : Hit efficiency for neutrons
- $\varepsilon_{distrib}$ .: 1 if in bulk matter,  $\frac{1}{2}$  for surfaces.

Focus of the talk:

- Determination of  $Y_n$  and  $\varepsilon_n$ .
- Allowed amounts of <sup>210</sup> Po for nEXO.

# Determining the neutron yields $Y_n$

• SOURCES-4C with some modifications:

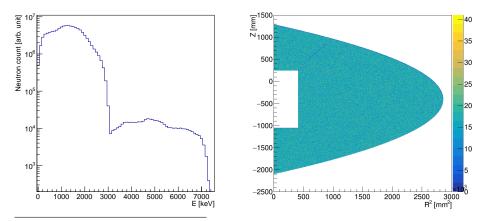
Comparison of neutron yield and mean energy between original and modified SOURCES-4C.

- Newer (α, n) cross-section data from JENDL-2005/AN and TENDL 2009.
- Energy range extended from 6.5 MeV to 15 MeV to accommodate higher-energy α's from <sup>218</sup>Po and <sup>214</sup>Po.
- Verified with numerical calculation using stopping power from the NIST ASTAR online database.

| Nuclide          | $\frac{Y_n^{mod}}{Y_n^{orig}}$ | $rac{\langle E_n^{mod}  angle}{\langle E_n^{orig}  angle}$ |
|------------------|--------------------------------|---|
| <sup>13</sup> C  | 1.05                           | 1.01  |
| <sup>17</sup> O  | 0.98                           | 1.002   |
| <sup>18</sup> O  | 1.01                           | 1.001   |
| <sup>19</sup> F  | 0.97                           | 0.99  |
| <sup>27</sup> Al | 1.23                           | 1.007   |
| <sup>29</sup> Si | 0.63                           | 0.935   |
| <sup>30</sup> Si | 0.58                           | 1.32  |

# Simulation result

Distributions of neutrons from  $(\alpha, n)$  in HFE<sup>\*</sup> in which the TPC is submerged.



\*HFE-7000, a cryogen by 3M with chemical formula  $C_3F_7OCH_3$ .

nEXO Rn daughter plateout

# Calculated neutron yields

| Plateout loca       | tion     | (0        | a, n) target   | Y <sub>n</sub> |
|---------------------|----------|-----------|--|----------------|
| Component           | Material | Component | Nuclides   | $[10^{-8}]$    |
| TPC vesse           | Cu       | HFE       | <sup>13</sup> C, <sup>17</sup> O, <sup>18</sup> O, <sup>19</sup> F   | 511            |
| HFE                 | HFE      | itself    | <sup>13</sup> C, <sup>17</sup> O, <sup>18</sup> O, <sup>19</sup> F   | 511            |
| Inner vessel liner  | Ti       | HFE       | <sup>13</sup> C, <sup>17</sup> O, <sup>18</sup> O, <sup>19</sup> F   | 511            |
| Field cage spacers  | Sapphire | itself    | <sup>17</sup> O, <sup>18</sup> O, <sup>27</sup> Al                   | 33.2           |
| SiPM                | Si       | itself    | <sup>29</sup> Si, <sup>30</sup> Si                                   | 7.3            |
| Charge tile backing | Quartz   | itself    | <sup>17</sup> O, <sup>18</sup> O, <sup>29</sup> Si, <sup>30</sup> Si | 6.7            |
| Interposer          | Quartz   | itself    | <sup>17</sup> O, <sup>18</sup> O, <sup>29</sup> Si, <sup>30</sup> Si | 6.7            |

• The neutron energy spectrum and their location of creation are used for the next step – the calculation of  $\varepsilon_n$ .

## Determining the hit efficiencies of neutrons $\varepsilon_n$

• GEANT4-based nEX0\_MC with modifications:

- "Shielding" physics list for high-precision low-energy hadronic interactions.
- Disabled radioactive decays in order to separate backgrounds due to <sup>137</sup>Xe decays from everything that happens before, such as inelastic scattering of neutrons.
- Neutron hit efficiency can be split into two terms:

$$\varepsilon_n = \varepsilon_{prompt} + \varepsilon_{n \to 137} \chi_e \cdot \varepsilon_{137} \chi_e$$

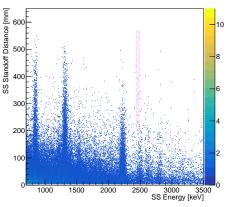
where

- ε<sub>prompt</sub>: Hit efficiency for prompt effects of neutrons
- $\varepsilon_{n \to 137Xe}$ : Probability for neutron capture anywhere in the active volume.
- $\varepsilon_{137Xe}$ : Hit efficiency for  $\beta$  decay of  $^{137}Xe$

### Neutron prompt effects

- "Prompt effects" include:
  - Neutron inelastic scattering on Xe, e.g. <sup>136</sup>Xe(n,n'γ)<sup>136</sup>Xe, <sup>134</sup>Xe(n,n'γ)<sup>134</sup>Xe.
  - Prompt gammas from neutron captures on nuclides, such as 2.2 MeV γ's from <sup>1</sup>H.
- Small background impact compared to <sup>137</sup>Xe.

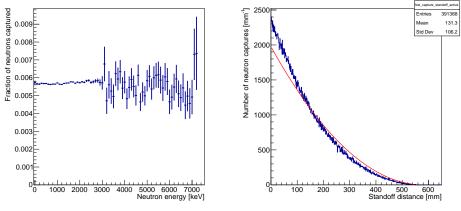




# Captures on <sup>136</sup>Xe of neutrons created in HFE

Neutron capture probability

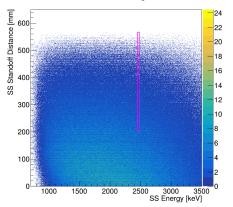
#### Uniformity of neutron captures



The red line shows a uniform standoff distribution.

# Hit efficiency of $^{137}{\rm Xe}\;\beta$ decays

- Since <sup>137</sup>Xe decays are localized, the positional distribution of <sup>137</sup>Xe decays should follow that of the neutron captures.
- Therefore, the distribution of  $^{137}$ Xe  $\beta$  decays is assumed to be uniform.
  - The hit efficiency of <sup>137</sup>Xe depends very weakly on position for decays within the field cage.
  - Outside the field cage, the hit efficiency of <sup>137</sup>Xe decays is substantially lower.
- The bias introduced by this assumption is expected to be small.



#### Xe137, ActiveRegion

#### Results

| Po210, HFE_Bu  | ılk                 | Po2  | 10, TPCVessel_HF           | E_Skin  | Po210, InnerCryo_Bulk   |
|--|---------------------|--|----------------------------|---|---|
| 600<br>100<br>100<br>100<br>100<br>100<br>100<br>100 | 5 3000 3500         | 10<br>10<br>10<br>10<br>10<br>10<br>10<br>10 | 1500 2000 2500<br>S S Smar | = 40<br>= 40<br>= 30<br>= 20<br>= 20<br>= 20<br>= 10<br>= 10<br>= 10<br>= 10<br>= 10<br>= 10<br>= 0<br>= 0 | 3<br>-2.5<br>-2<br>-1.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br>-1<br>-0.5<br> |
| Component  | Yn                  | εn   | Area/Mass                  | Bkg. impact   | Allowed <sup>210</sup> Po activity †  |
|  | [10 <sup>-8</sup> ] | $[10^{-4}]$                                  | $[m^{2}]$                  | [(c/y)/(Bq/m <sup>2</sup> )]  | [Bq/m <sup>2</sup> ]  |
| TPC Vesse  | 511                 | 1.9  | 7.84                       | 0.12  | 0.0047  |
| SiPMs  | 7.3                 | 2.1  | 11.43                      | $2.8 \times 10^{-3}$  | 0.20  |
| Interp oser  | 6.7                 | 2.0  | 11.43                      | $2.4 	imes 10^{-3}$   | 0.22  |
| Field cage spacers                                   | 33.2                | 2.1  | 0.5                        | $5.5 \times 10^{-4}$  | 1.0   |
| Charge tile backing                                  | 6.7                 | 1.7  | 2.54                       | $4.6 \times 10^{-4}$  | 1.1   |
| IV liner   | 511                 | $7.2 \times 10^{-4}$                         | 40.72                      | $2.4 	imes 10^{-4}$   | 2.4   |
|  | [10 <sup>-8</sup> ] | [10-4]                                       | [kg]                       | [(c/y)/(Bq/kg)]   | [µBq/kg]  |
| HFE  | 511                 | 0.2  | 31814                      | 103   | 58  |

 $\dagger_{\rm HFE}$  is allocated 6.25  $\times$  10^{-3} of the total background, the rest 6.25  $\times$  10^{-4} each.

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nEXO Rn daughter plateout

# Conclusion

Summary

- We have estimated the background impact of radon daughter plateout to nEXO.
- Based on the estimates, we have allocated background budgets to the components that are more susceptible to this background.
- While it is not expected to be a major background source, we need to devise ways to measure <sup>210</sup>Po contamination on surfaces and in bulk volumes.

More presentations related to this topic:

- Dmitry Chernyak, Radon daughter plate-out as a background source in nEXO experiment.
- Isaac Arnquist, Exploration of Methods to Remove Implanted Pb-210 and Po-210 Contamination from Silicon Surfaces

## Talks and posters by nEXO collaborators

- Dmitry Chernyak, Radon daughter plate-out as a background source in nEXO experiment
- Isaac Arnquist, Exploration of Methods to Remove Implanted Pb-210 and Po-210 Contamination from Silicon Surfaces
- Venkatesh Veeraraghavan, <sup>42</sup>Ar background in nEXO
- Brian Mong, Improving nEXO Sensitivity with Radon Distillation
- Khadouja Harouaka, Sample preparation strategies for ultra-trace assay of actinides in difficult samples matrices
- Amanda French, Use of QQQ-ICP-MS for Ultra Low Background Measurements
- Andreas Piepke, The nEXO Background Control Program
- Douglas Leonard, Facilities and Recent Developments for Radioactivity Assay at CUP
- Richard Saldanha, Ultra-low background flexible cables
- Eric Hoppe, Update on Electroforming Plans and Facilities





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Backups

#### Backups

# SOURCE-4C checks

Neutron yield:

$$Y_n(E_\alpha) = \frac{N_A}{M_T} \cdot \int_0^{E_\alpha} \frac{\sigma(E)}{P_m(E)} \ dE$$

where  $E_{\alpha}$  is the initial alpha energy,  $N_A$  is the Avogadro's number,  $M_T$  is the molar mass of the target material,  $\sigma(E)$  is the  $(\alpha, n)$  cross-section, and  $P_m(E)$  is the stopping power per unit density.

Comparison between original and modified SOURCES-4C with numerical calculation.

| Target           | $Y_n$ for $^{210}$ Po $lpha$ 's [10 $^{-6}$ ] |       |       |  |
|------------------|---|-------|-------|--|
| material         | Orig.   | Mod.  | Num.  |  |
| HFE <sup>‡</sup> | 5.3   | 5.1   | 4.3   |  |
| Sapphire         | 0.28  | 0.33  | 0.31  |  |
| SiPM             | 0.12  | 0.073 | 0.074 |  |